

Effects of Iron Conduits  
On Line Drop

F. A. Putt  
B. E. Beamer

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An investigation of the  
effects of iron conduits on









AN INVESTIGATION OF THE  
EFFECTS OF IRON CONDUITS ON LINE DROP.

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A THESIS PRESENTED

BY

F. A. PUTT.

B. E. BEAMER.

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AN INVESTIGATION OF THE  
EFFECTS OF IRON CONDUITS ON LINE DROP.

The tendency in central station practice has been to decrease the cost of generation of energy ,and to cut down the losses wherever it was possible so that at the present time the attention has been directed to the investigation of and diminishing , of any loss which decreases the efficiency and output of the central station. In large central stations a loss or leakage of energy amounting to only a fraction of one per cent of the total power developed , will in the course of a year mean a loss of hundreds and sometimes thousands of dollars to the company. This fact has led to the investigation of losses in the transmission of energy , and in connection with this the effect of iron conduit on line drop when the iron conduit is used in alternating current work.

It is current practice in central stations to place the leads from the generators, rotary converters , and transformers to the switchboard in iron conduits. This is also true of substation wiring as well as of the wiring in large buildings.

It is the object of this paper to investigate and discuss the effect of the iron conduit on the line drop and experimentally determine the magnitude of the losses due to it.



It is a well known fact that when direct current is used the iron pipe or conduit would have no effect on the line drop and the only difference of potential would be caused by the ohmic resistance of the wire. When alternating current is used there maybe a noticeable drop due to the self-induction of the wire.

One of the fundamental principles of electricity is that when a conductor carries an electric current there is a field set up around that conductor proportional to the current. Any change in this field will produce a counter electromotive force in the conductor proportional to the rate of change of the flux. This counter- electromotive force acts as a resistance opposing the flow of the current in the conductor. When the conductor is enclosed in the iron conduit the flux is increased due to the increased permeability of the iron over air; thereby increasing the counter- electromotive force and thus causing a larger drop over the wire.

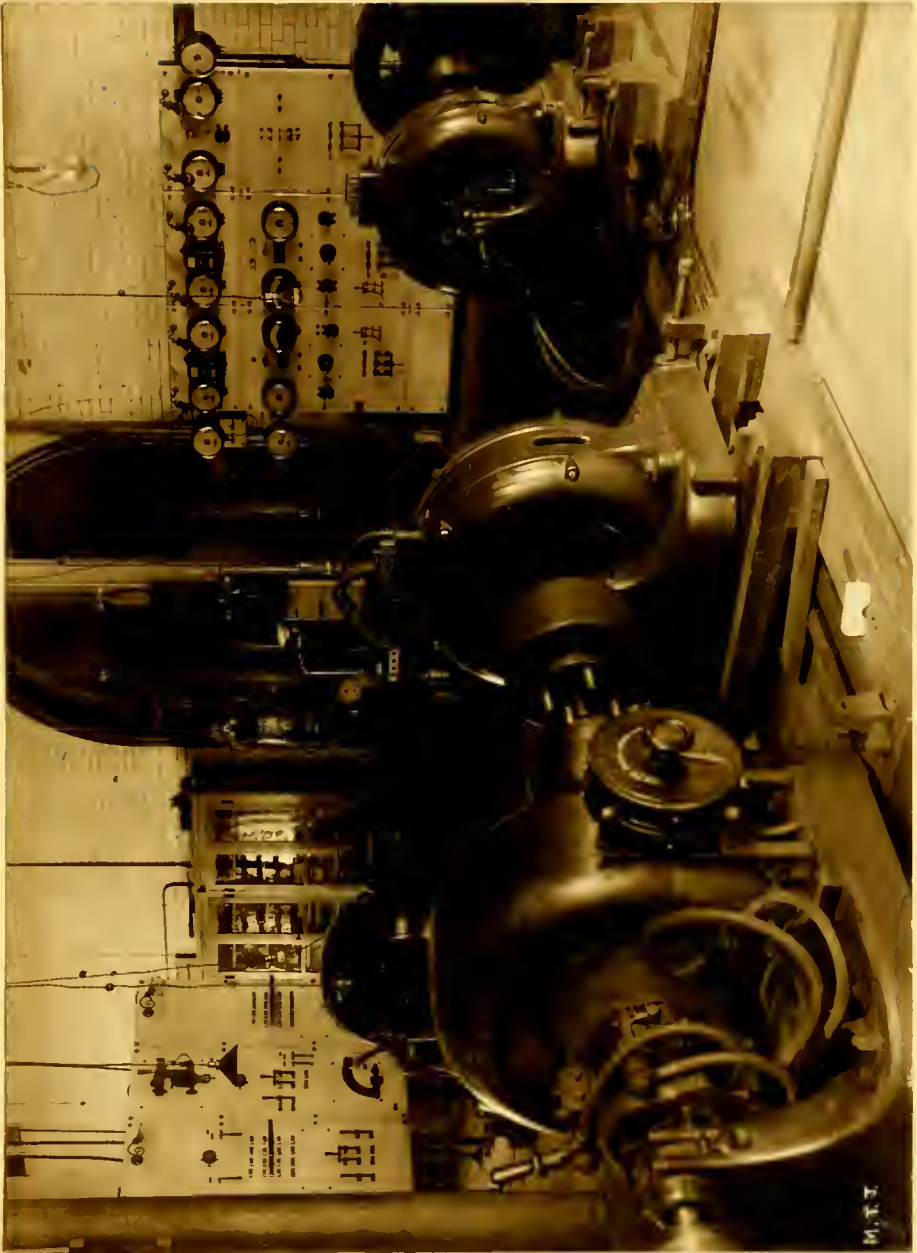
Experiments along this line were carried on with single and three phase currents under different conditions of load, variation of frequency , and conduits.

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### Description of The Apparatus Used.

The following machines and instruments were used in obtaining the data for this paper. The alternating current both single and three-phase , for fifty(50) , fifty-five (55) , and sixty (60) cycles was obtained from a General Electric Company three-phase alternating current generator # 65447- six pole -- giving seventy-two (72) amperes at twelve hundred (1200) revolutions per minute and one hundred and twenty (120) volts at full load. The alternator was driven by a direct - connected Crocker- Wheeler motor # 265 rated for twenty - six (26) horse power at one thousand twenty-five revolutions per minute ; taking one hundred and ninety (190) amperes at one hundred and fifteen (115) volts. The generator was excited by current from a Westinghouse compound direct current generator # 208697 rated at one hundred and twenty-five (125) volts -- one hundred and twenty (120) amperes at one thousand fifty (1050) revolutions per minute, driven a direct - connected twenty-six (26) horse power Crocker- Wheeler motor. This method of excitation afforded good regulation for all condition of load and frequency.

For all data at twenty-five and thirty cycles, single and three-phase currents was taken on a direct-driven Wood alternator rated at thirty horse power , one hundred and ten (110) volts and five hundred (500) revolutions per minute.

The following table shows the results of the tests obtained for the three types of the generator. The generator was run at 1000 rpm and the load was varied from 0 to 1000 watts. The results are given in the following table:

Load (watts)	Current (amps)	Voltage (volts)	Power Factor
0	0	0	0
100	1.0	100	0.95
200	2.0	200	0.95
300	3.0	300	0.95
400	4.0	400	0.95
500	5.0	500	0.95
600	6.0	600	0.95
700	7.0	700	0.95
800	8.0	800	0.95
900	9.0	900	0.95
1000	10.0	1000	0.95

The results show that the generator is capable of producing 1000 watts of power at 1000 rpm and a power factor of 0.95. The voltage is proportional to the current and the power factor is constant.

The load was obtained by means of an incandescent lamp rack and so assured a non-inductive load .

Thomson alternating current ammeters and voltmeters calibrated for this experiment were used to measure the current and pressure respectively. A Weston wattmeter was used to measure the power consumed and a Queen electro-dynamometer calibrated to read in volts was used to measure the drop over the wire in the pipes.

The different frequencies were obtained by running the alternators at different speeds . A Weston tachometer was used to indicate the speed.

used to indicate the speed.

The different frequencies were obtained by varying the distance of the different objects. A special arrangement

was made over the side of the ship.

As the ship moved forward the sound waves were reflected back to the observer and the time taken for the sound to return was measured. The distance of the object was then calculated from the time taken for the sound to return and the speed of sound.

The time taken for the sound to return was measured by a chronometer. The distance of the object was then calculated from the time taken for the sound to return and the speed of sound.



SCHEME #1 SINGLE PHASE







### Single-Phase.

#### Method:-

The authors first investigated the drop over the wire in the conduit when single phase current was used. The apparatus was connected as shown in the scheme (#1) on the preceeding page. The lamp rack used for the load was connected in series with the wire in the pipe, and an ammeter and the series coil of the wattmeter . The voltmeter was connected across the line , reading the drop over the wire in the pipes, and the lamp rack. The pressure coil of the wattmeter was connected to the same points as the voltmeter.

The electro-dynamometer was connected to read the drop over the wire in the pipe . Eighty feet of (# 14) number fourteen rubber covered copper wire was used being doubled in forty feet of one and one eighth inch iron conduit.

Runs were taken with the wire in the pipe for twenty-five , thirty, fifty , fifty-five, and sixty cycles. The voltage was maintained constant at one hundred and ten (110) volts over the lamps. Simultaneous readings were taken of the drop over the wire in the pipe by means of the dynamometer and watts consumed in the circuit, by the wattmeter for loads varying from ten to fifty amperes by five ampere steps. The wire was then removed from the iron conduit and similiar readings taken for the same frequencies and loads.



## Single-phase Data. Wire in the Pipe.

60 cycles.			55 cycles.			50 cycles.		
Amp.	K.W.	Volts.	Amp.	K.W.	Volts.	Amp.	K.W.	Volts.
11.5.	1.1	.8	11.5	1.1	.8	10.4	1.1	.67
15.5	1.6	1.32	15.5	1.6	1.32	14.5	1.6	1.3
19.5	2.2	1.8	18.5	2.1	1.7	18.4	2.1	1.74
24.	2.6	2.2	22.3	2.62	2.14	23.	2.6	3.2
29.	3.2	2.72	28.	3.2	2.6	27.4	3.15	2.6
33.	3.6	3.15	32.	3.7	3.	32.	3.7	3.03
37.5	4.25	3.65	36.2	4.2	3.5	36.5	4.2	3.5
41.5	4.8	4.15	40.5	4.75	3.95	40.5	4.75	3.98
46.	5.2	4.55	45.	5.25	4.5	45.	5.2	4.48
48.5	5.5	4.9	49	5.72	4.9	49.	5.7	4.87

30 cycles.			25 cycles.		
Amp.	K.W.	Volts.	Amp.	K.W.	Volts.
10.5	1.	.8	10.5	1.	.66
15.	1.5	1.3	14.8	1.5	1.25
19.2	2.08	1.8	19.	2.1	1.8
24.	2.6	2.2	24.	2.62	2.2
29.	3.14	2.7	28.8	3.18	2.65
33.4	3.72	3.14	34.	3.63	3.1
38.	4.22	3.6	38.	4.2	3.7
42.	4.73	4.1			
46.5	5.28	4.6			

1909			1910			1911		
1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1
1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2
1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3
1.4	1.4	1.4	1.4	1.4	1.4	1.4	1.4	1.4
1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
1.6	1.6	1.6	1.6	1.6	1.6	1.6	1.6	1.6
1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7
1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8	1.8
1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9
2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0
2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1
2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4
2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6
2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7
2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8
2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9
3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0

1909			1910		
1.1	1.1	1.1	1.1	1.1	1.1
1.2	1.2	1.2	1.2	1.2	1.2
1.3	1.3	1.3	1.3	1.3	1.3
1.4	1.4	1.4	1.4	1.4	1.4
1.5	1.5	1.5	1.5	1.5	1.5
1.6	1.6	1.6	1.6	1.6	1.6
1.7	1.7	1.7	1.7	1.7	1.7
1.8	1.8	1.8	1.8	1.8	1.8
1.9	1.9	1.9	1.9	1.9	1.9
2.0	2.0	2.0	2.0	2.0	2.0
2.1	2.1	2.1	2.1	2.1	2.1
2.2	2.2	2.2	2.2	2.2	2.2
2.3	2.3	2.3	2.3	2.3	2.3
2.4	2.4	2.4	2.4	2.4	2.4
2.5	2.5	2.5	2.5	2.5	2.5
2.6	2.6	2.6	2.6	2.6	2.6
2.7	2.7	2.7	2.7	2.7	2.7
2.8	2.8	2.8	2.8	2.8	2.8
2.9	2.9	2.9	2.9	2.9	2.9
3.0	3.0	3.0	3.0	3.0	3.0



## Single- phase Data . Wire out of Pipe.

60 cycles.			55 cycles.			50 cycles.		
Amp.	K.W.	Volts.	Amp.	K.W.	Volts.	Amp.	K.W.	Volts.
10.5	1.1	.5	12.5	1.2	.64	12.5	1.	.9
14.8	1.52	1.2	16.5	1.5	1.3	16.5	1.55	1.34
19.	2.05	1.64	20.8	2.05	1.74	20.7	2.1	1.73
24.	2.62	2.1	25.	2.6	2.12	25.	2.6	2.15
29.	3.2	2.55	30.	3.15	2.6	30.	3.13	2.54
33.	3.7	2.94	34.2	3.65	3.	34.2	3.68	3.
37.5	4.2	3.4	38.8	4.15	3.47	39.	4.21	3.55
42.4	4.6	3.84	43.5	4.66	3.9	43.2	4.7	3.9
47.	5.1	4.4	47.5	5.17	4.39	47.5	5.2	4.35
51.	5.6	4.78	51.	5.62	4.7	51.	5.6	4.73

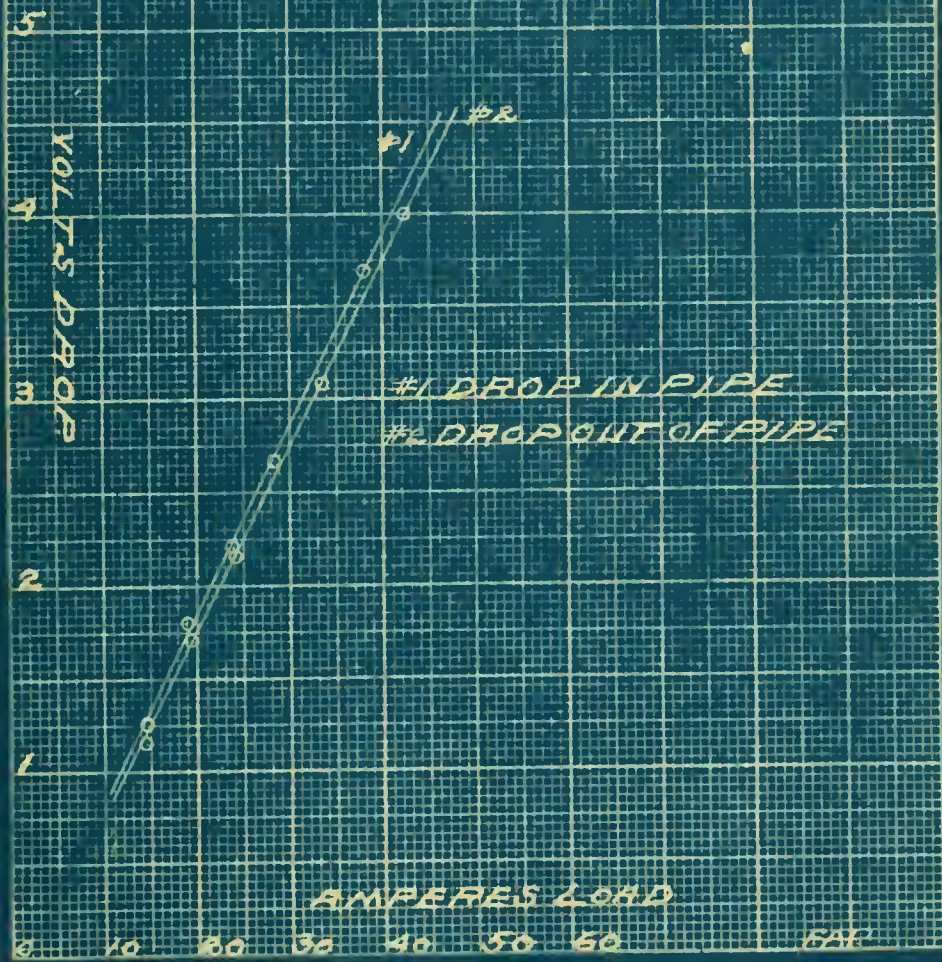
30 cycles.			25 cycles.		
Amp.	K . W .	Volts.	Amp.	K . W .	Volts.
10.5	1.62	.62	10.5	1.1	.56
14.6	1.5	1.3	14.6	1.5	1.25
19.2	2.08	1.7	19.2	2.1	1.72
24.	2.62	2.15	24.	2.63	2.18
28.8	3.18	2.6	28.7	3.2	2.65
33.	3.7	3.	33.2	3.7	3.07
38.	4.23	3.5	37.6	4.2	3.58
42.4	4.8	4.	42.5	4.8	4.
46.8	5.3	4.5			

1950-1951			1951-1952			1952-1953		
Year	Area	Yield	Year	Area	Yield	Year	Area	Yield
1950	100	1.00	1951	100	1.00	1952	100	1.00
1951	100	1.00	1952	100	1.00	1953	100	1.00
1952	100	1.00	1953	100	1.00	1954	100	1.00
1953	100	1.00	1954	100	1.00	1955	100	1.00
1954	100	1.00	1955	100	1.00	1956	100	1.00
1955	100	1.00	1956	100	1.00	1957	100	1.00
1956	100	1.00	1957	100	1.00	1958	100	1.00
1957	100	1.00	1958	100	1.00	1959	100	1.00
1958	100	1.00	1959	100	1.00	1960	100	1.00
1959	100	1.00	1960	100	1.00	1961	100	1.00
1960	100	1.00	1961	100	1.00	1962	100	1.00
1961	100	1.00	1962	100	1.00	1963	100	1.00
1962	100	1.00	1963	100	1.00	1964	100	1.00
1963	100	1.00	1964	100	1.00	1965	100	1.00
1964	100	1.00	1965	100	1.00	1966	100	1.00
1965	100	1.00	1966	100	1.00	1967	100	1.00
1966	100	1.00	1967	100	1.00	1968	100	1.00
1967	100	1.00	1968	100	1.00	1969	100	1.00
1968	100	1.00	1969	100	1.00	1970	100	1.00
1969	100	1.00	1970	100	1.00	1971	100	1.00
1970	100	1.00	1971	100	1.00	1972	100	1.00
1971	100	1.00	1972	100	1.00	1973	100	1.00
1972	100	1.00	1973	100	1.00	1974	100	1.00
1973	100	1.00	1974	100	1.00	1975	100	1.00
1974	100	1.00	1975	100	1.00	1976	100	1.00
1975	100	1.00	1976	100	1.00	1977	100	1.00
1976	100	1.00	1977	100	1.00	1978	100	1.00
1977	100	1.00	1978	100	1.00	1979	100	1.00
1978	100	1.00	1979	100	1.00	1980	100	1.00
1979	100	1.00	1980	100	1.00	1981	100	1.00
1980	100	1.00	1981	100	1.00	1982	100	1.00
1981	100	1.00	1982	100	1.00	1983	100	1.00
1982	100	1.00	1983	100	1.00	1984	100	1.00
1983	100	1.00	1984	100	1.00	1985	100	1.00
1984	100	1.00	1985	100	1.00	1986	100	1.00
1985	100	1.00	1986	100	1.00	1987	100	1.00
1986	100	1.00	1987	100	1.00	1988	100	1.00
1987	100	1.00	1988	100	1.00	1989	100	1.00
1988	100	1.00	1989	100	1.00	1990	100	1.00
1989	100	1.00	1990	100	1.00	1991	100	1.00
1990	100	1.00	1991	100	1.00	1992	100	1.00
1991	100	1.00	1992	100	1.00	1993	100	1.00



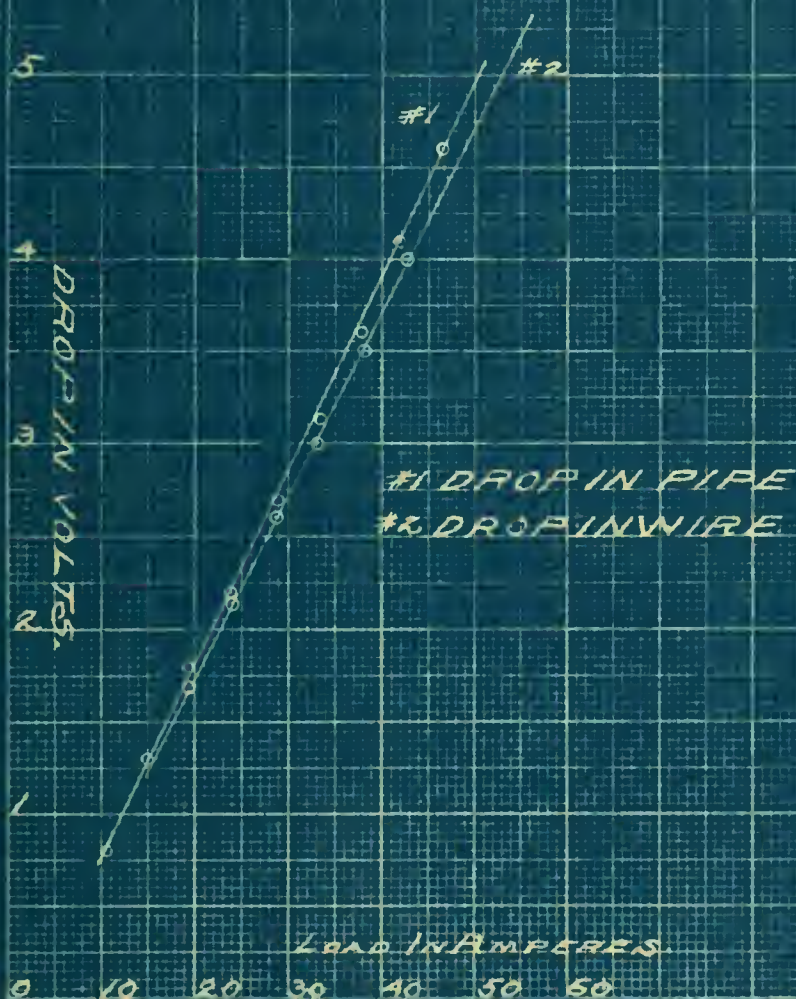
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# SINGLE-PHASE - 25 CYCLES





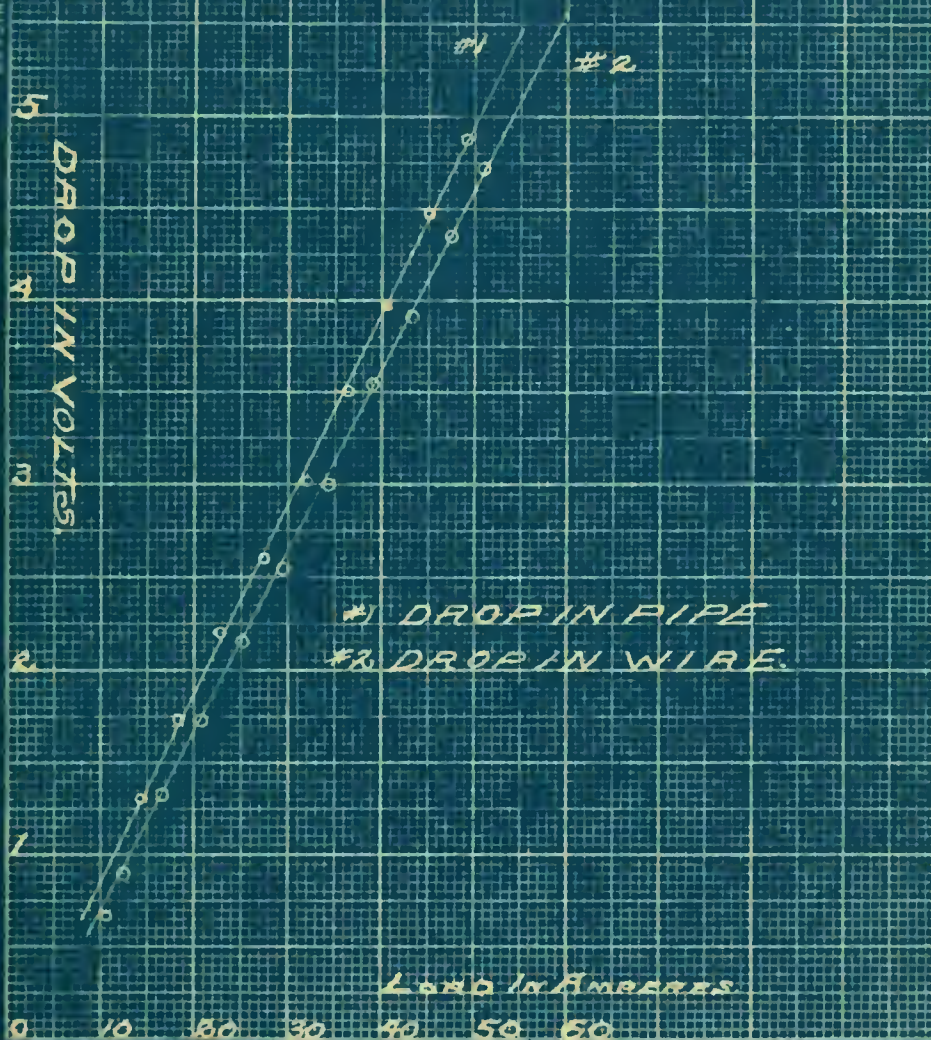
SINGLE-PHASE - 30 CYCLES.







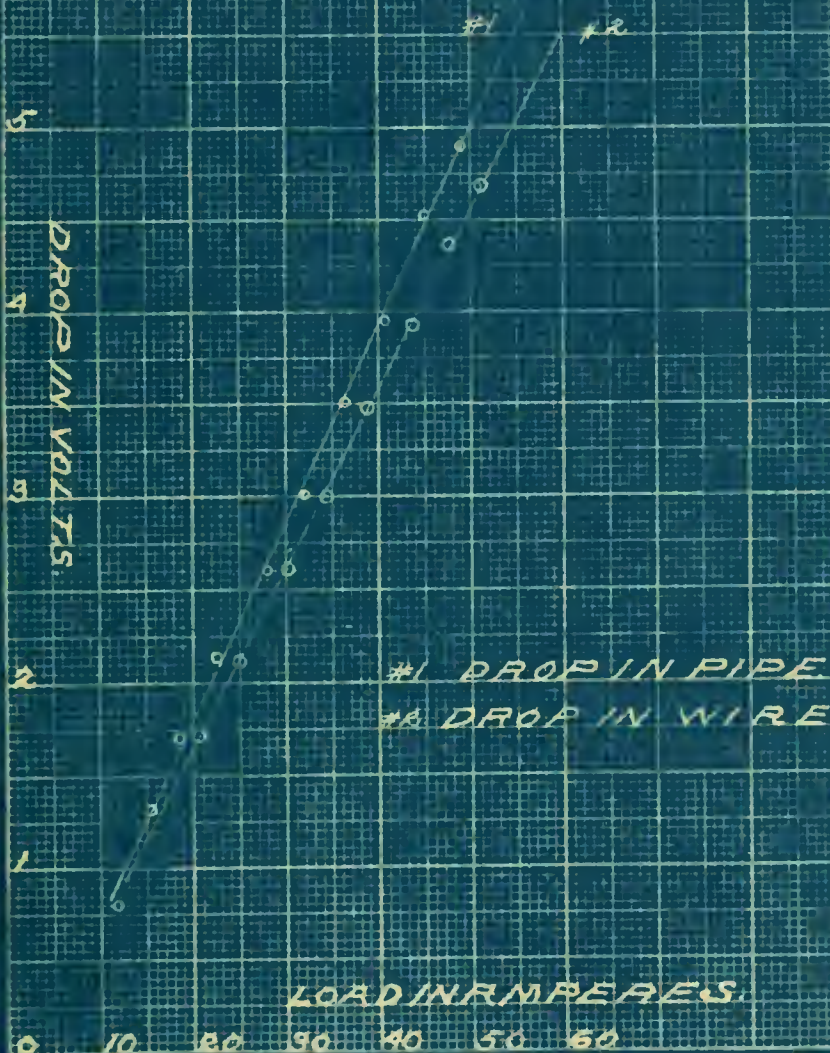
# SINGLE-PHASE-50 CYCLES







# SINGLE-PHASE 55 CYCLES





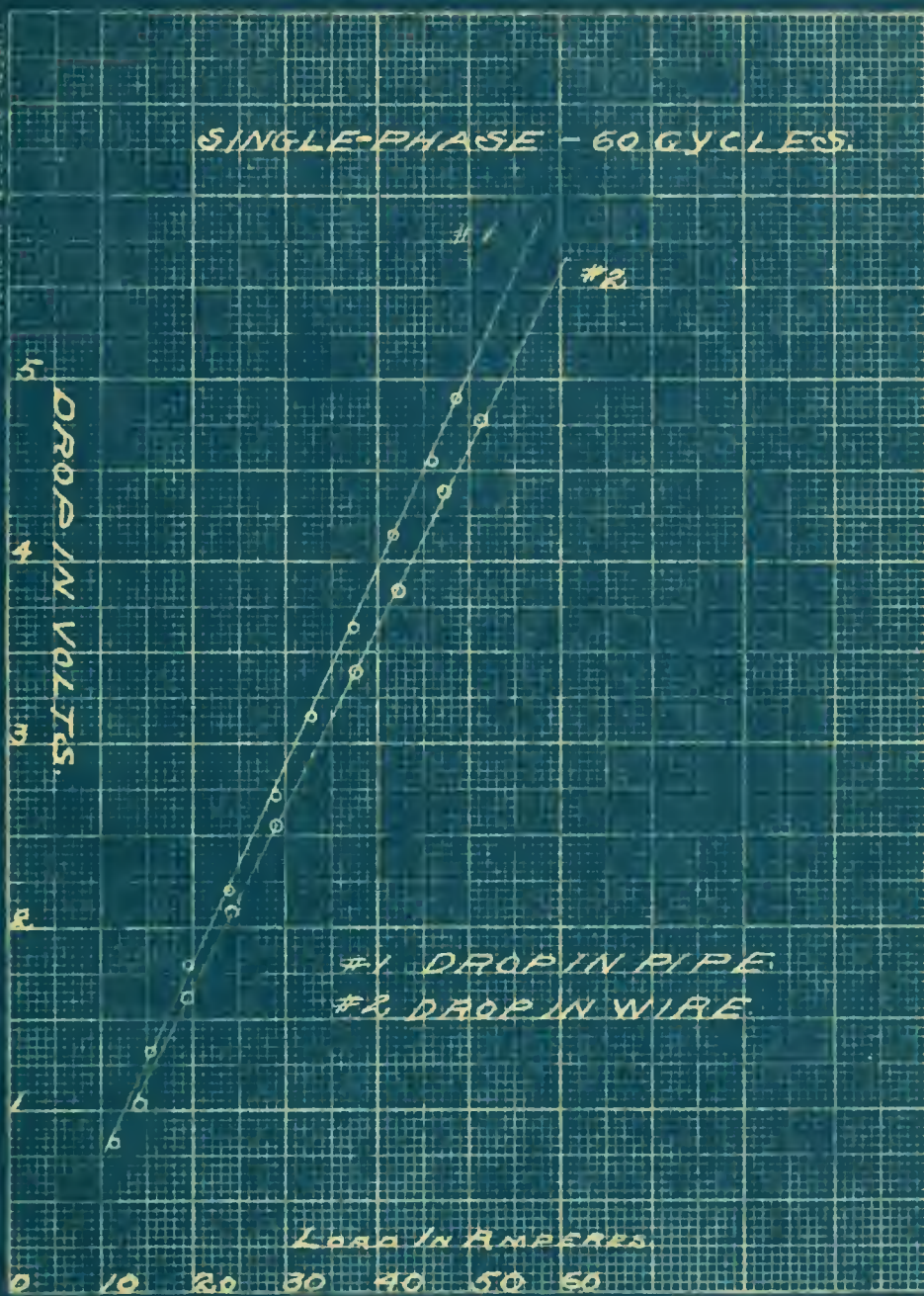
# SINGLE-PHASE - 60 CYCLES.

DROP IN VOLTS.

#1 DROP IN PIPE  
#2 DROP IN WIRE

LOAD IN AMPERES

0 10 20 30 40 50 60













### Three- Phase.

#### Method:-

Determination of the drop in the pipe when three wires and three-phase currents were used with balanced load.

The apparatus used for the determination of the above was connected as shown in scheme #2 given on the preceeding page. Three leads of number fourteen rubber- covered copper wire each seventy-five feet long were placed in seventy-five feet of one and one eighth inch conduit. These are represented in the scheme as extending from points 1-2; 3-4; and from 5-6 respectively. Points 1-3-5- represent a universal switch by means of which the ammeter and wattmeter could be placed in series with any one of the lines.

There were two pressure terminals on this switch. One of these pressure terminals was connected in series with a sliding contact which could be rotated , making contact with either of the other phases as was desired. A delta connection was used on the lamp racks as shown in the scheme.

Care was taken to keep the load balanced , one bank of lamps on each rack being placed in the circuit for each reading. The pressure over each phase was maintained constant at one hundred and ten (110) volts and loads of from ten to fifty-five amperes were used.

Simultaneous readings of ammeter, voltmeter, and electro-dynamometer were taken for each load with the wires in the pipe and at the different frequencies.



The wires were then taken from the pipe and the experiment repeated , readings being taken with the different loads and frequencies as before.

... ..  
... ..  
... ..  
... ..  
... ..



## Three-phase . Wire in the pipes.

60 cycles.

55 cycles.

50 cycles.

Amp.	K.W.	Volts.	Amp.	K.W.	Volts.	Amp.	K. W.	Volts.
17.8	1.55	1.35	18.	1.6	1.54	17.4	1.55	1.52
25.	2.25	2.	25.8	2.4	2.12	25.8	2.31	2.08
33.	3.1	2.84	33.8	3.3	2.84	33.	3.06	2.8
40.	3.8	3.55	45.7	4.3	4.05	40.5	3.7	3.42
		4.24					4.31	
47.2	4.53	4.24	51.5	4.7	4.75	47.5		4.13
							5.	
						54.		4.9

30 cycles.

25 cycles.

Amp.	K .W.	Volts.	Amp.	K .W.	Volts.
17.4	1.55	1.52	17.4	1.55	1.5
25.5	2.32	2.09	25.4	2.31	2.04
33.	3.05	2.78	33.	3.05	2.8
40.	3.68	3.42	40.	3.7	3.41
46.8	4.27	4.06	47.	4.3	4.08
			54.	5.	4.8

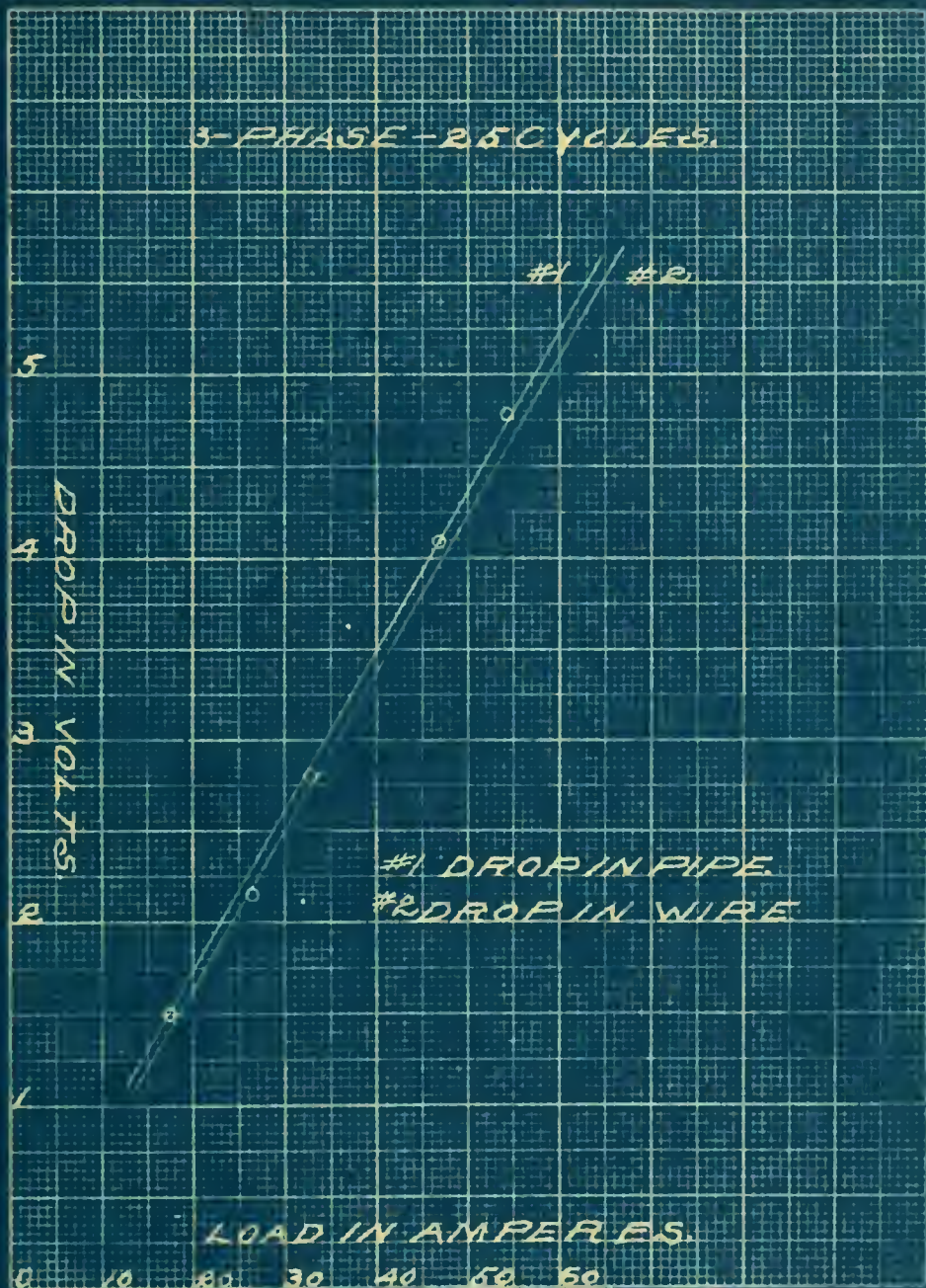


## Three-phase Data. Wire out of the pipes.

60 cycles.			55 cycles.			50 cycles.		
Amp.	K . W.	Volts.	Amp.	K.W.	Volts.	Amp.	K.w.	Volts.
18.	1.6	1.38	18.	1.6	1.46	12.6	1.65	1.28
26.	2.38	2.	26.5	2.4	2.1	25.7	2.4	2.
33.8	3.15	2.6	34.	3.22	2.7	33.2	3.24	2.6
42.	3.92	3.4	42.	4.	3.38	40.6	3.97	3.2
49.5	4.75	4.12	49.	4.7	4.15	47.8	4.7	3.9
56.2	5.37	4.82	53.2	5.22	4.55	55.2	5.45	4.64

30 cycles.			25 cycles.		
Amp.	K . W	Volts.	Amp.	K . W .	Volts.
17.8	1.6	1.5	18.	1.6	1.5
26.6	2.4	2.1	26.2	2.4	2.14
34.	3.2	2.78	34.	3.2	2.78
42.	3.9	3.48			
49.2	4.7	4.2			
57.3	5.52	5			

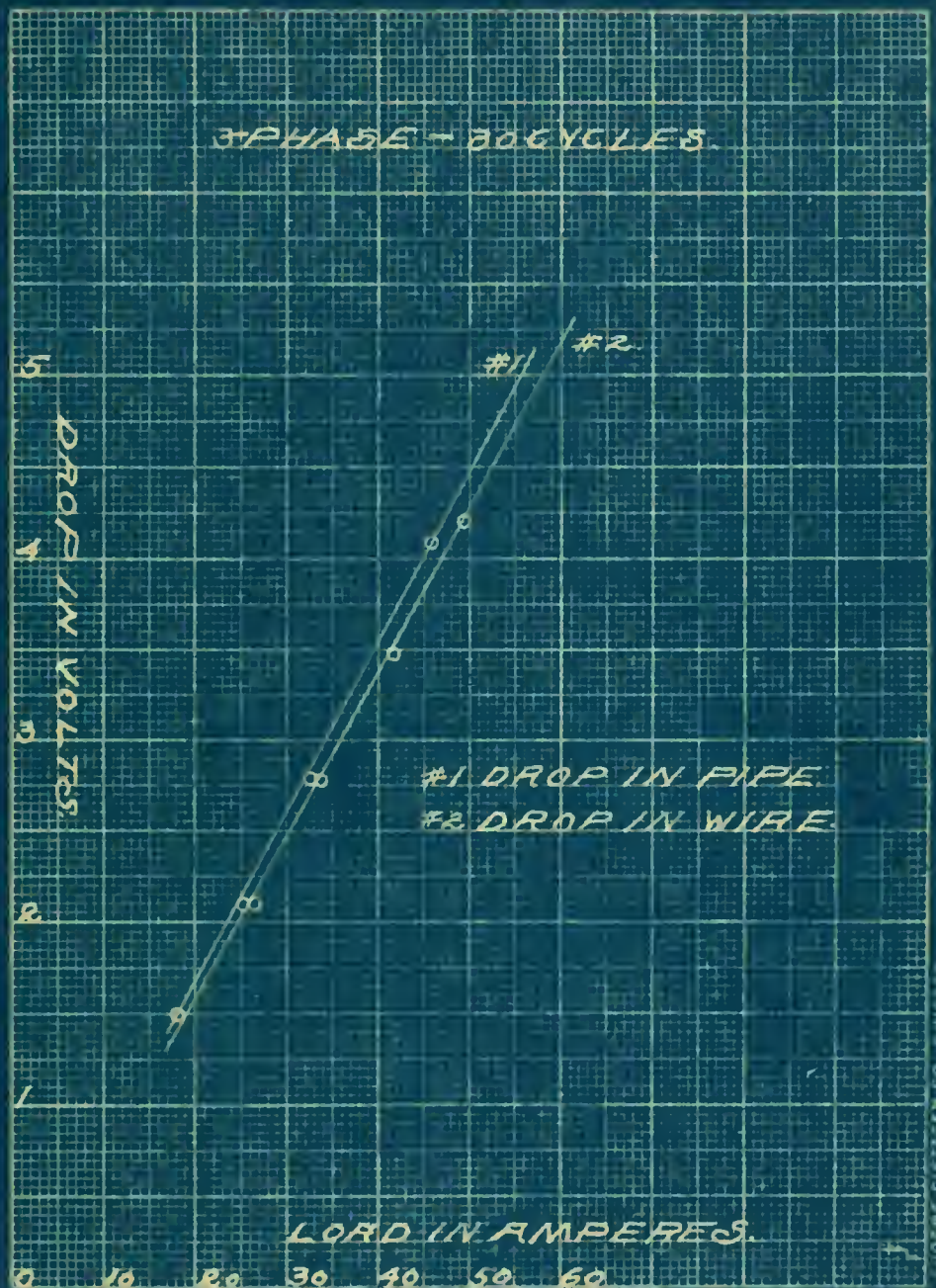




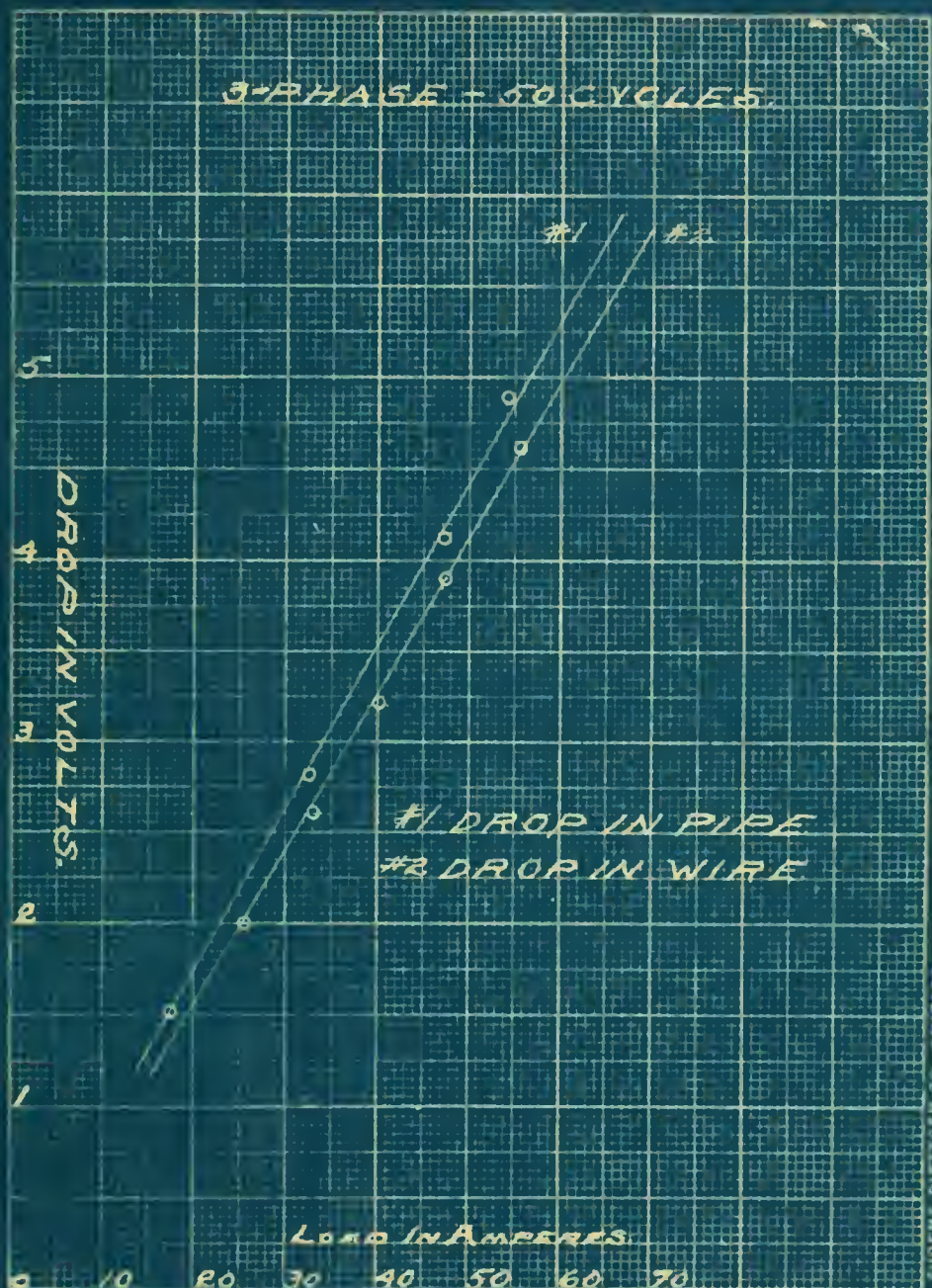
LOCATED BY THE U.S. AIR FORCE







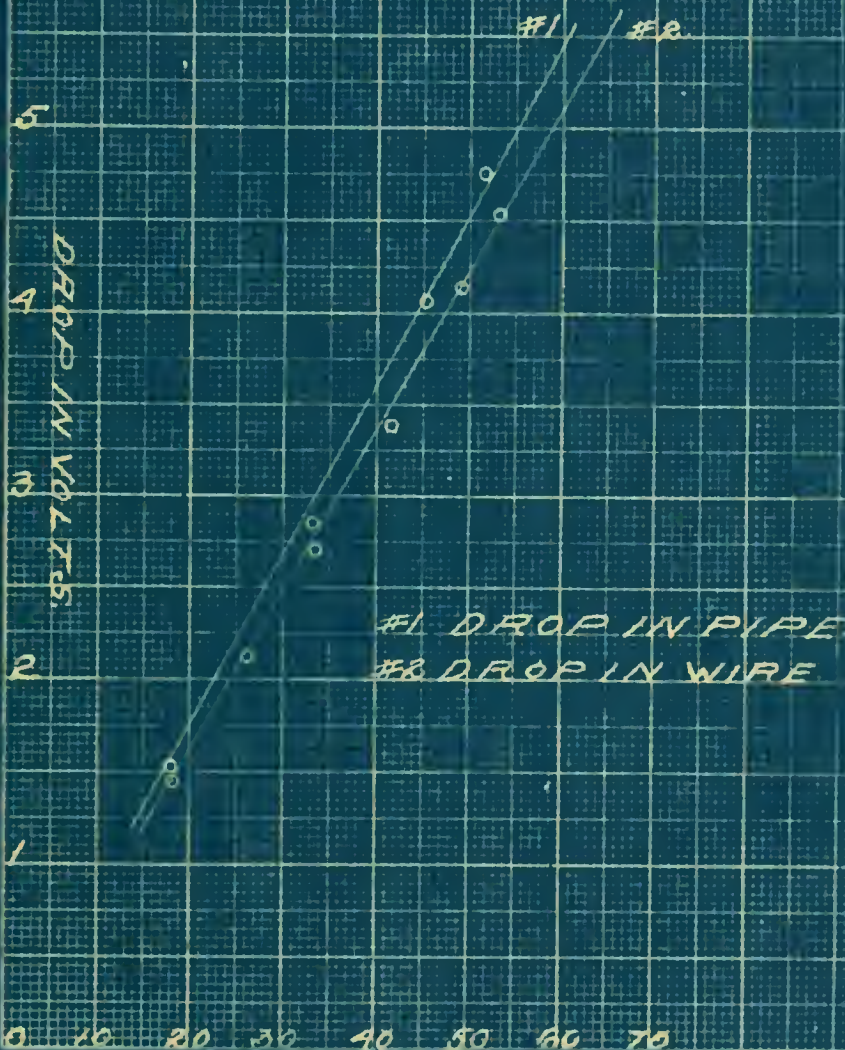




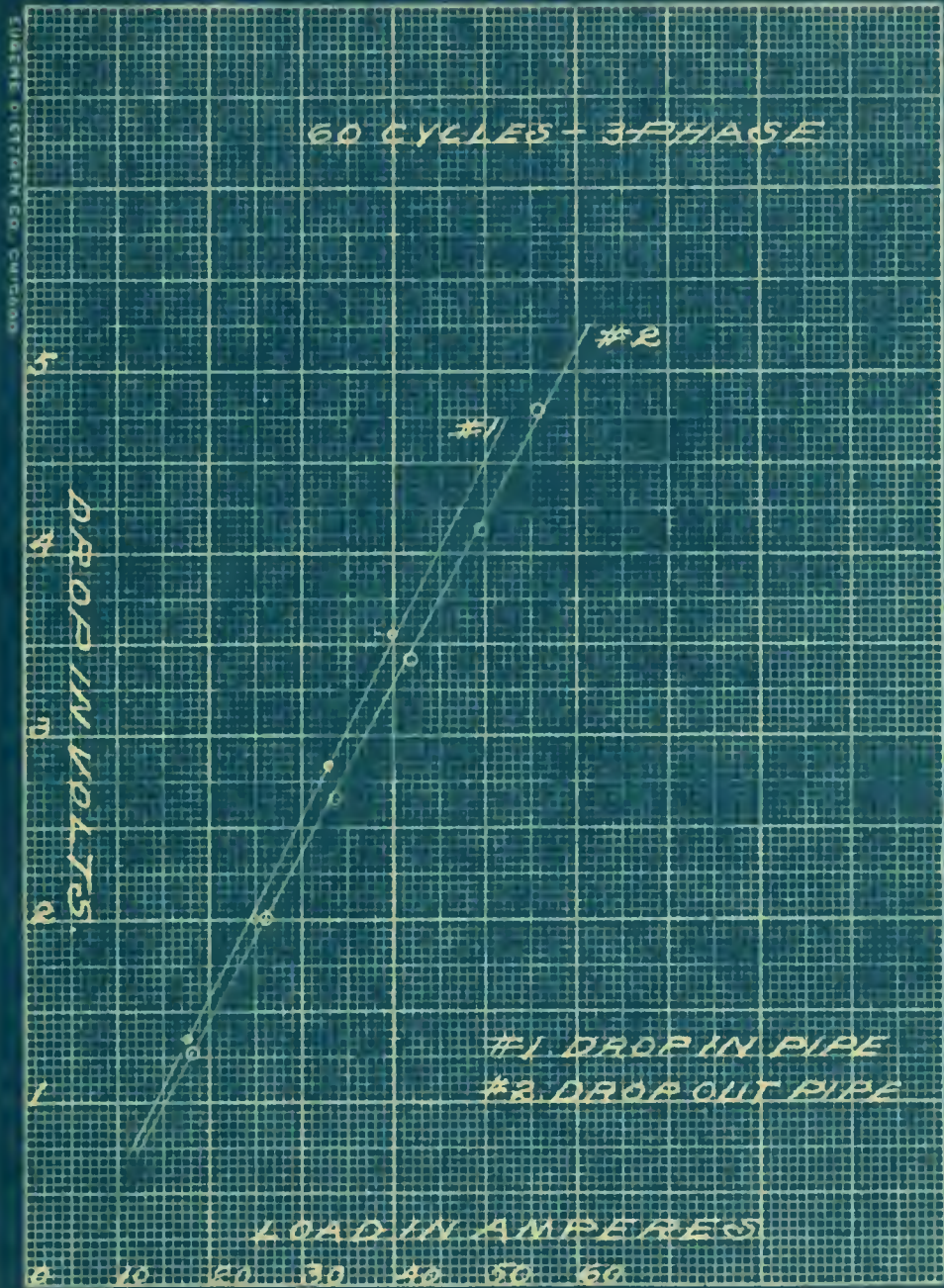




3-PHASE - 50 CYCLES











## EFFECT OF FREQUENCY ON LINE DROP WITH CONSTANT LOAD/

Single- Phase.			
	.40 Amperes.	45 Amperes.	50 Amperes.
Cycles.	Volts.	Volts.	Volts.
25	3.86	4.4	4.92
30	3.88	4.42	4.94
50	3.91	4.45	4.97
55	3.92	4.48	5.
60	3.94	4.5	5.02

## Three- Phase.

	40 Amperes.	50 amperes.
Cycles.	Volts.	Volts.
25	3.5	4.35
30	3.53	4.4
50	3.55	4.45
55	3.57	4.5
60	3.58	4.52



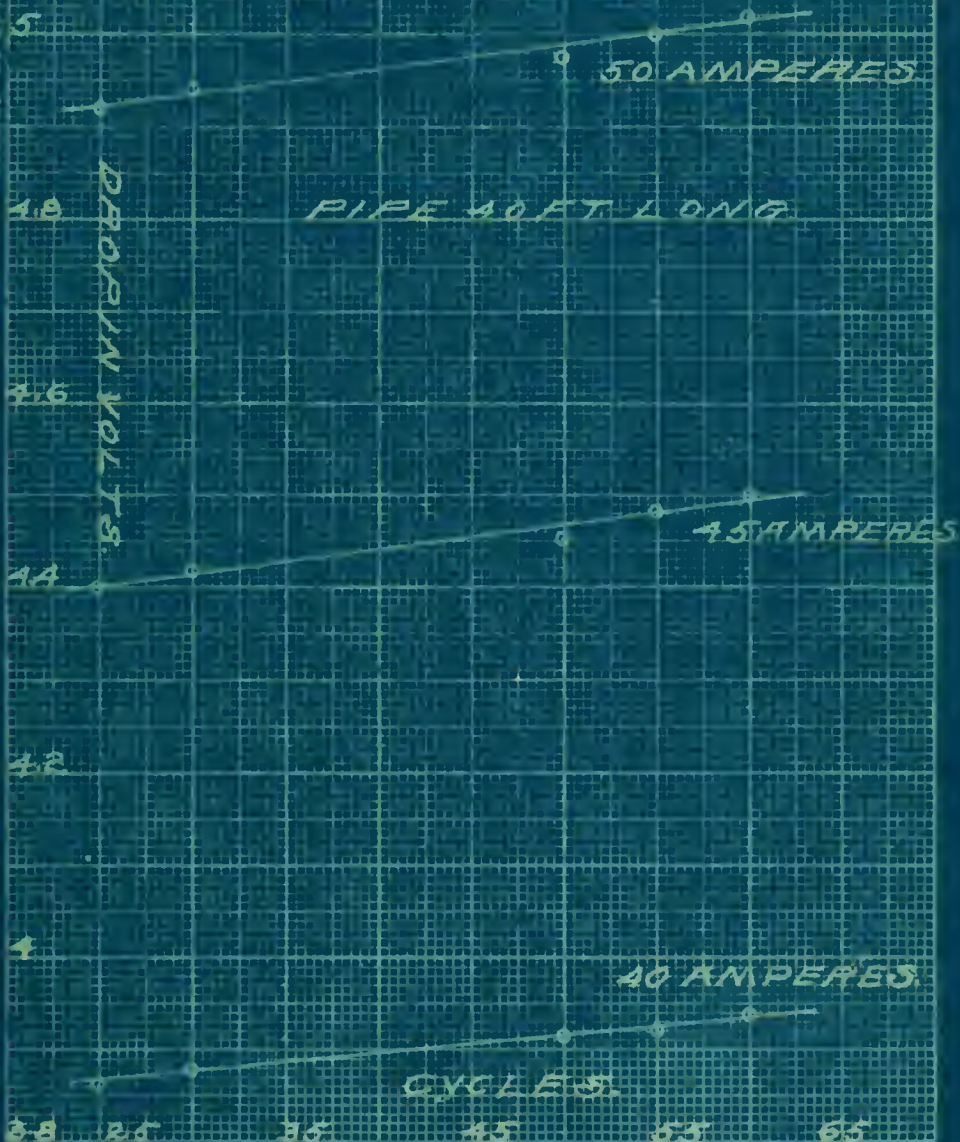
# REPORT ON THE PROGRESS OF THE WORK DURING THE YEAR 1900

RESEARCHES ON THE PHYSICAL PROPERTIES OF THE SUBSTANCE		RESEARCHES ON THE CHEMICAL PROPERTIES OF THE SUBSTANCE	
TEMPERATURE	DETERMINATION OF THE	TEMPERATURE	DETERMINATION OF THE
100	1.00	100	1.00
200	1.00	200	1.00
300	1.00	300	1.00
400	1.00	400	1.00
500	1.00	500	1.00
600	1.00	600	1.00

## RESEARCHES ON THE PHYSICAL PROPERTIES OF THE SUBSTANCE

TEMPERATURE	DETERMINATION OF THE	TEMPERATURE	DETERMINATION OF THE
100	1.00	100	1.00
200	1.00	200	1.00
300	1.00	300	1.00
400	1.00	400	1.00
500	1.00	500	1.00
600	1.00	600	1.00

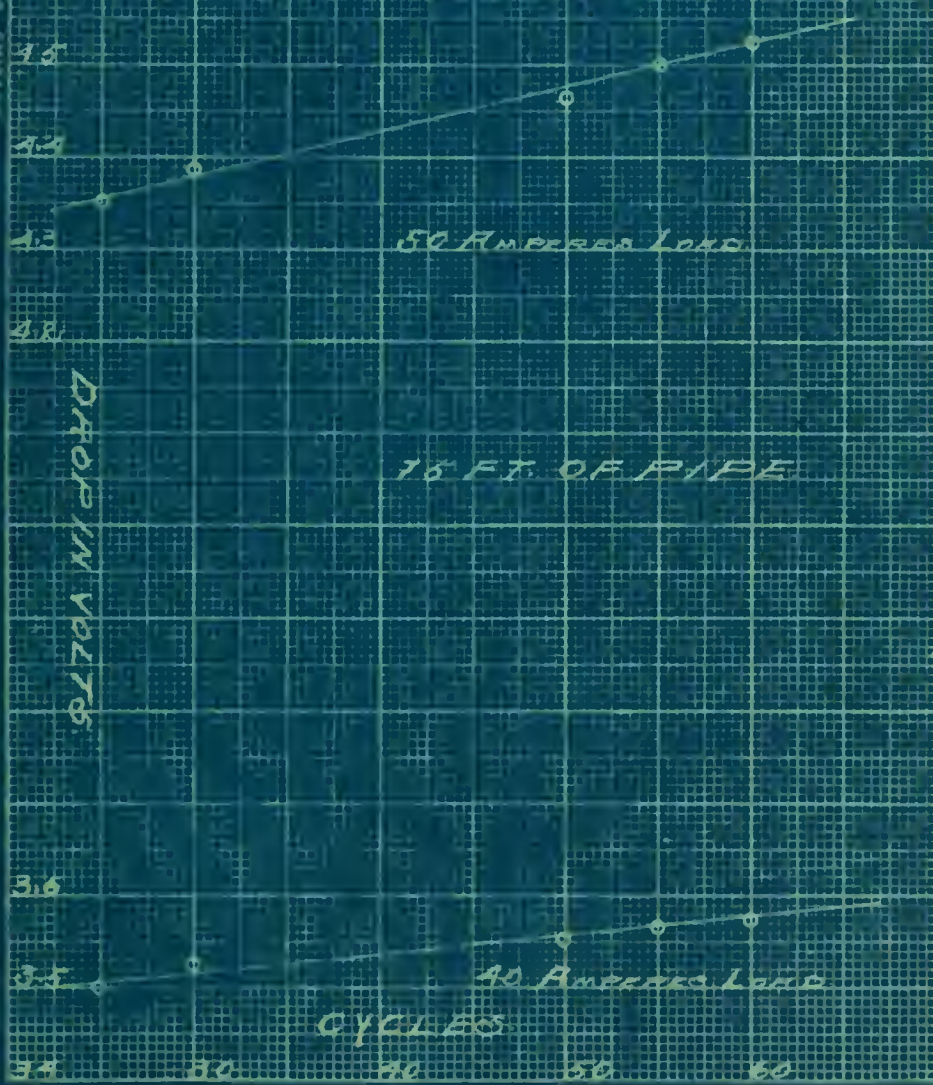
# EFFECT OF FREQUENCY ON DROP IN PIPE SINGLE-PHASE CONSTANT LOAD





WAGNER ELECTRIC CO. CHICAGO

# EFFECT OF FREQUENCY ON DROP IN PIPE THREE PHASE CONSTANT LOAD









## CALIBRATION OF INSTRUMENTS.

Weston Wattmeter.  
#1791

WATTS.

True	Indicated
1	1
2	2.02
3	3.01
4	3.98
5	5.04
6	6.02
7	6.98
8	8.04
9	9.04
10	10.08
11	11.07

THOMSON A. C. AMMETER.  
#70511  
AMPERES.

True	Indicated.
10.	10
17.	15
21.5	20
26.5	25
31.	30
36.8	35
41.	40
46.	45
50.2	50
55.	55
60.	60

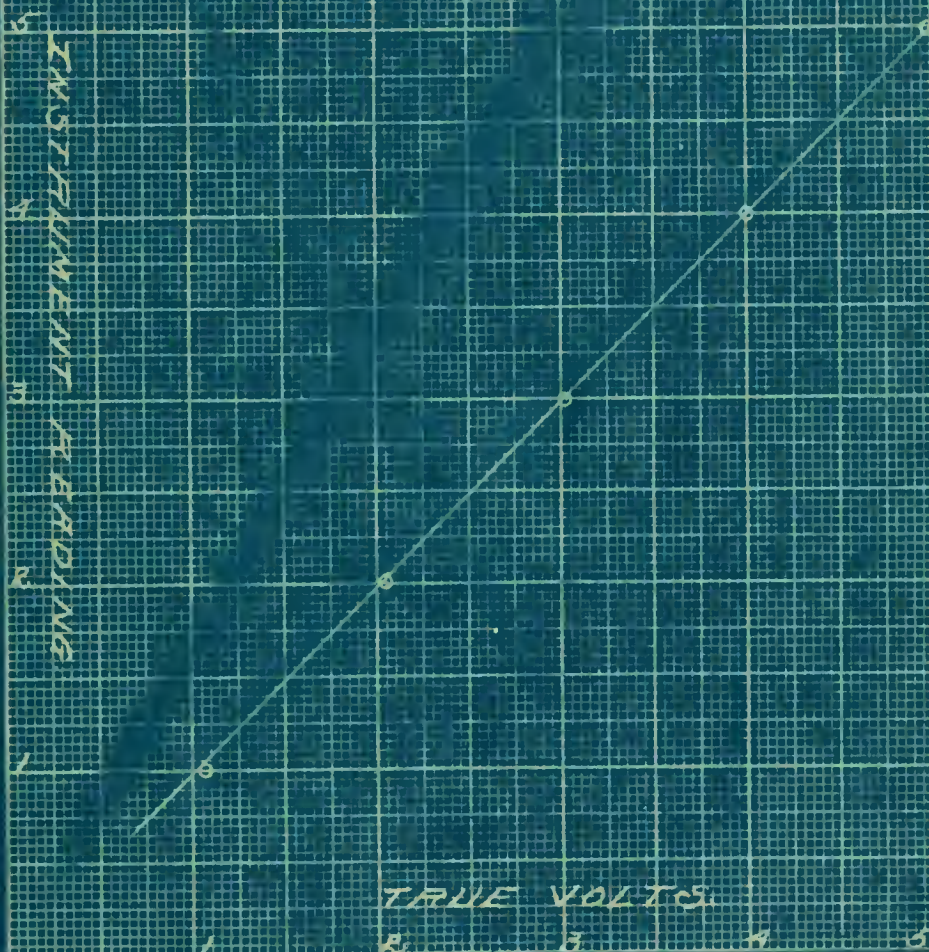
QUEEN ELECTRODYNAMOMETER. (0-5)

VOLTS

True	Indicated.
1.	.98
1.5	1.47
2.	1.98
2.5	2.48
3.	2.99
3.5	3.5
4.	4.
4.5	4.5

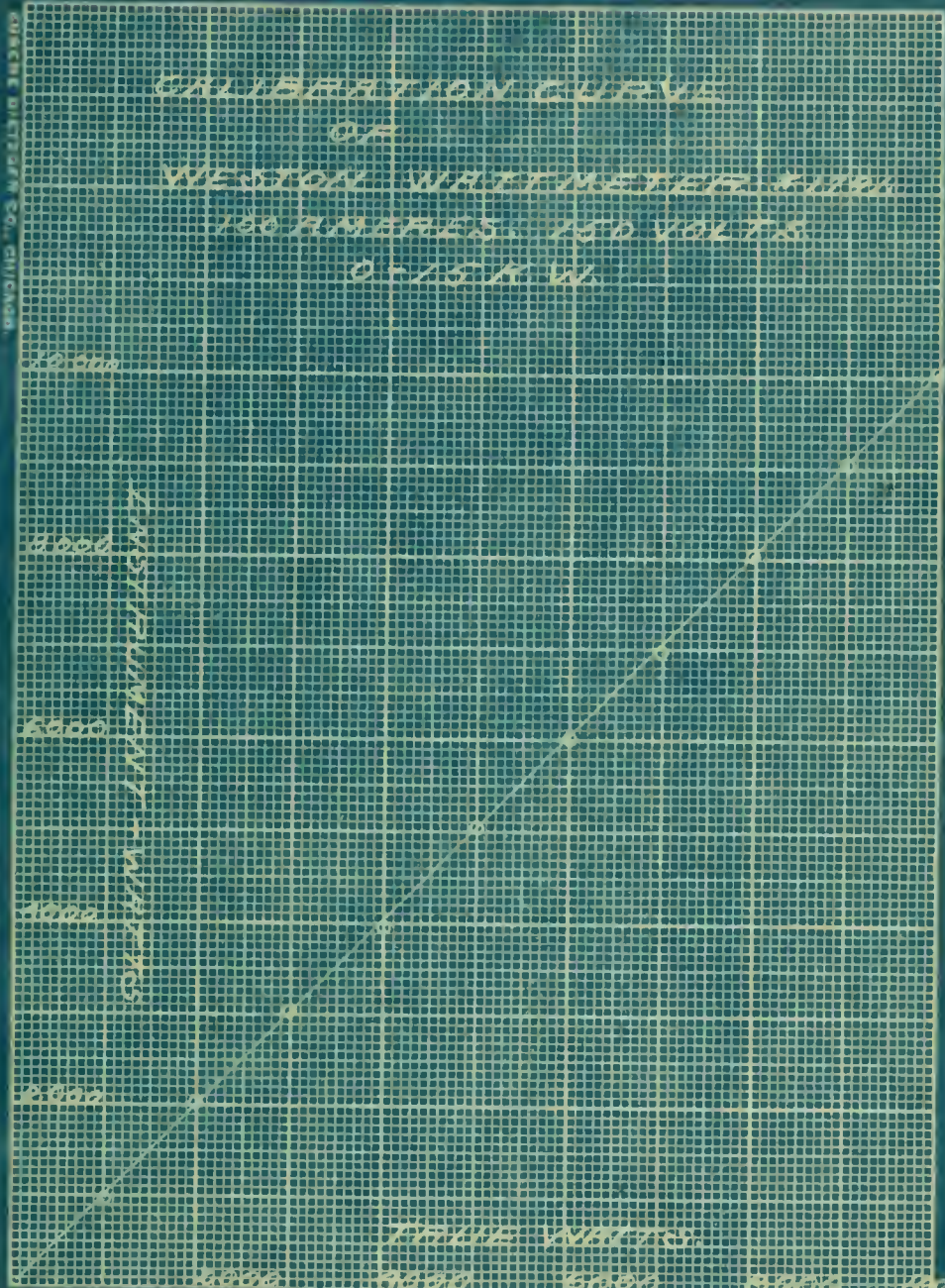


# Calibration Curve of Weston Dynamometer-Voltmeter (0-5)









UNITED STATES GOVERNMENT

1964

1965

1966

1967

1968

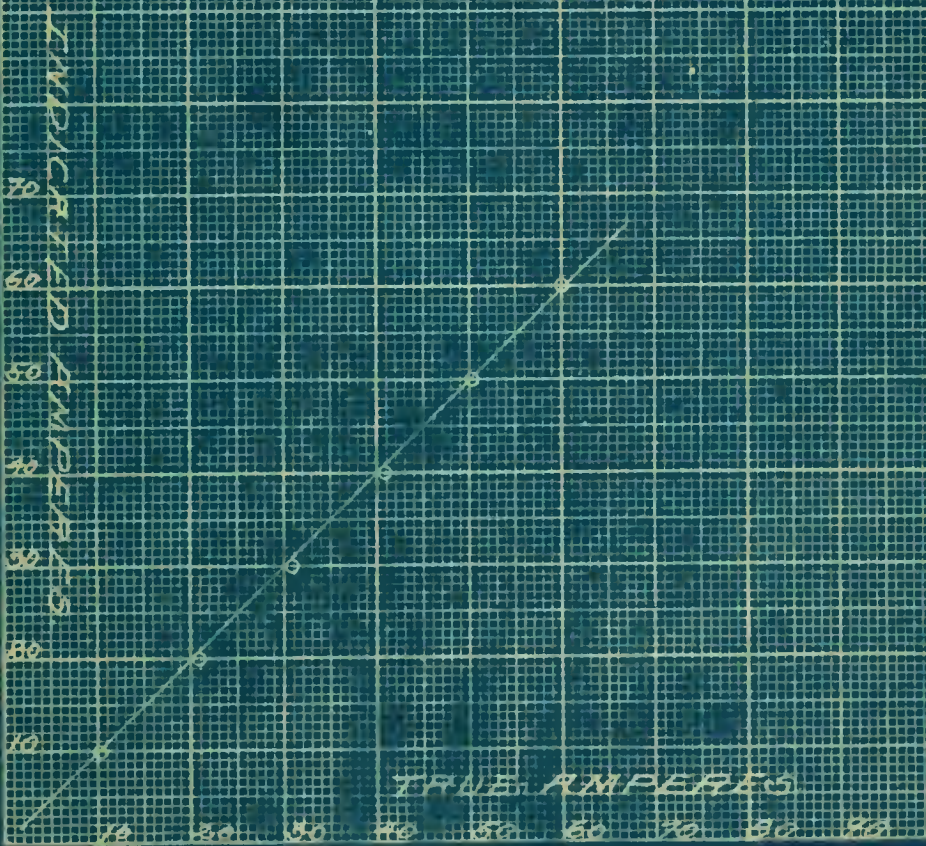
1969





EUGENE DISTRICT CO. CHICAGO

CALIBRATION CURVE  
 WESTON A.C. AMMETER #70511  
 (0-100) AMPERES.





### Explanation of data and curves.

Curves were platted from the data obtained to show graphically the difference between the drop over the wire when in the conduit and when outside of it.

The curves on pages ten to fourteen inclusive were platted from data taken with single-phase current. Curve #1 being the drop over the wire in the pipe and curve #2 showing the drop over the wire when the conduit was not used. In the same way the curves on pages twenty to twenty-four were platted from the data taken with three-phase current.

The data on page twenty-five showing the effect of frequency on line drop was taken from the curves of variable load. From this data the curves on pages twenty-six and twenty-seven were platted.

The instruments used were carefully and accurately calibrated and curves platted from the data obtained and included in this paper on pages twenty)Nine to thirty-one inclusive.





## DISCUSSION.

By a comparison of the data and the curves previously given it can be seen that the iron conduit has a very marked effect upon the difference of potential over the wire, increasing it very noticeably.

This increase in apparent resistance would be too small in value to be read on the average central station instrument. It is even very small when compared with the ohmic resistance of the wire.

From the data and curves of the single and three-phase currents, the authors find that the self-induction due to the use of the iron conduit has a greater effect for single phase currents. With the three-phase current and three wires in the conduit the fields caused by the current in the separate conductors would oppose each other. Since the currents are not in the same phase and therefore do not reach a maximum at the same time their fields neutralizing each other cutting down the self-induction.

The effect of different cyclic speeds was compared and it was found that the effect of self-induction increased directly as the frequency. The effect also increased directly as the load.

The same length of wire in the conduit was used in each case and the temperature at which the readings were taken



was kept as uniform as possible.

The wire used is the smallest wire found in construction work and the most available for this investigation. It furnishes a sample of what the effect would be if larger wire were used and a proportionately larger current.

With a load of fifteen amperes which is about the normal load for number fourteen wire on covered work the increased load at sixty cycles single phase is about one tenth of a volt. The ohmic drop at this load was one and two tenths volts making the drop due to self-induction one twelfth of the ohmic drop.

The effect of self-induction would increase directly with the length of the iron conduit used, and one tenth of a volt for seventy five feet would mean .133, volts per hundred feet or 1.33 volts per thousand feet. With of fifteen amperes and sixty cycles with three phase currents the difference in voltage was .08 for seventy five feet of wire. This made the inductive drop on fifteenth of the ohmic drop. The drop per hundred feet would be .106 volts and per thousand feet of wire in the conduit would be 1.06 volts.

The induction of the wire in the conduit would be increased if where there are a number of circuits different wires of different phases put together. To avoid this it is wise to see that wires of the same phase are put in the same pipe and thus cut down the

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effect of induction to a minimum. This is especially true in the wiring of large buildings.

If the wire is wound together as tightly as possible the induction will be reduced as well as the capacity of a pipe increased. With concentric wires the effect of self-induction will be reduced to zero. The induction in the wire besides causing an increase drop in potential would also cause a large amount of heating of the iron which might reach dangerous limits if not reduced.

FINIS.



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